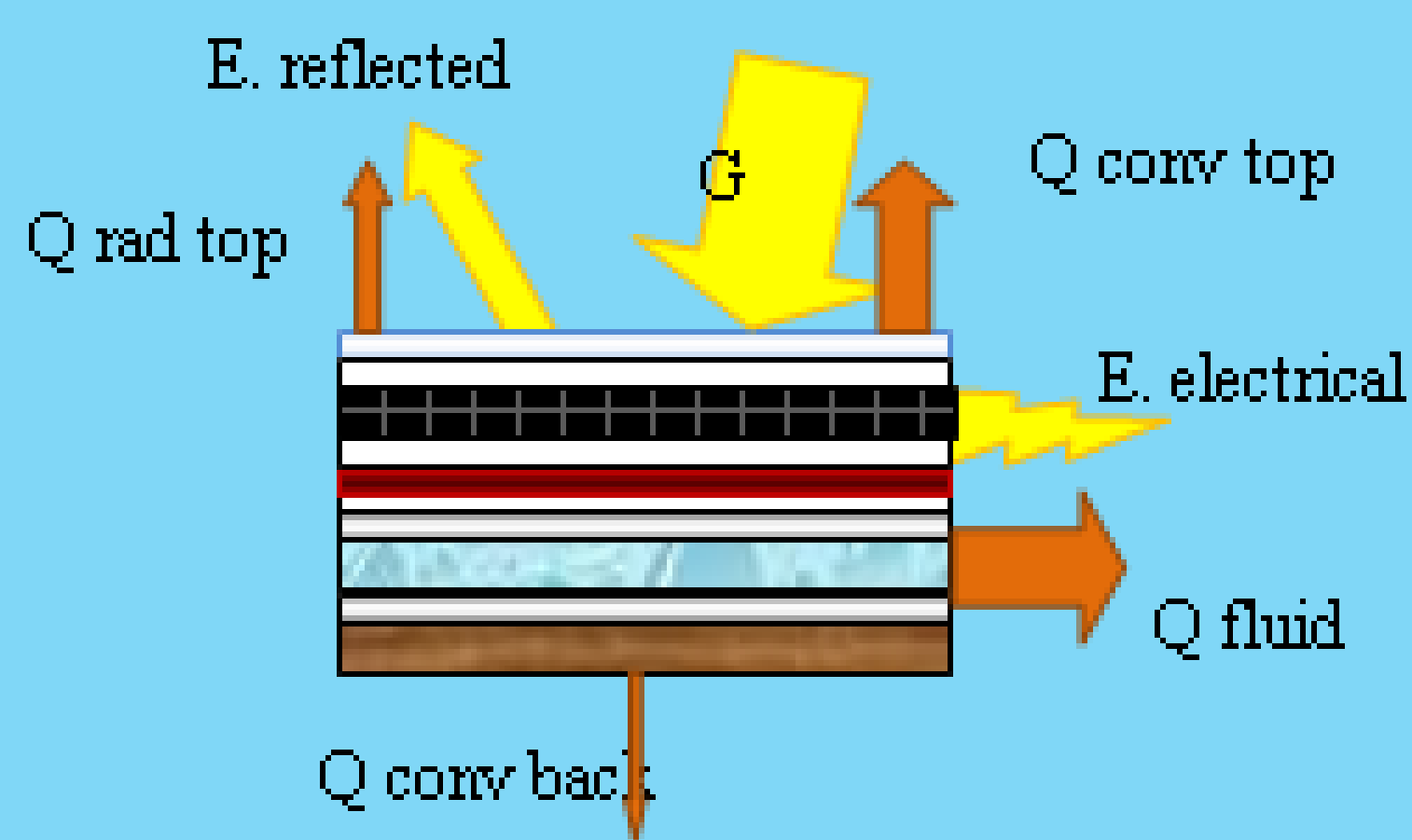


Experimental Validation of 1D model for photovoltaic/ thermal (PV/T) modules

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Numerical PV/T model

An energy balance for a quasi 1D simplified model



Symbol	Meaning	Units
A, B, C and D	Coefficients depending on module characteristics	
Cp	Heat capacity	W/kg/K
G	Solar irradiation	W/m ²
H	Global coefficient	W/m ² /K
h _{RAD}	Radiative coefficient	W/m ² /K
H _{WIND}	Convective coefficient on top plate due to the wind	W/m ² /K
H _{FLUID}	Convective coefficient on the plate due to the water	W/m ² /K
m	Water Flow rate	L/s
T	Temperature	K
V _{WIND}	Wind velocity	m/s
Width	Width of solar collector	m
X	Water flow direction	
t _a	Transmittance-absorption on diffuse, direct and horizontal irradiation	-
η _{PV}	Electrical efficiency	-
η _{TH}	Thermal efficiency	-

$$(\tau_g) \cdot G \cdot (1 - \eta_{PV}(G, T_{PV})) = h_{RAD}(T_{PV}) \cdot (T_{PV}(x) - T_{SKY}) + H_{TOP}(V_{WIND}) \cdot (T_{PV}(x) - T_A) + H_{FLUID} \cdot (T_{PV}(x) - T_F(x)) \quad (eq. 1)$$

$$H_{FLUID} \cdot (T_{PV}(x) - T_F(x)) = H_{BACK} \cdot (T_F(x) - T_{BACK}) + \dot{m} \cdot Cp \cdot \frac{dT_F}{dx} \quad (eq. 2)$$

Module outlet temperature and electrical power are then deduced thanks to an iterative approach on photovoltaic temperature (T_{PV}).

$$T_{F,OUT} = (T_{F,IN} - C) \times e^{-D \cdot Width} + C \quad (eq. 3)$$

$$T_{PV} = A \times T_{F,MEAN} + B \quad (eq. 4)$$

Subscript	Meaning
A	Ambient
BACK	Between fluid and rear surface
F	Fluid
FLUID	Between PV cells and fluid
PV	Photovoltaic cells
TOP	Between cells and ambient

In non-null flow rate cases, equations were simplified (Solar Keymark standard directives)

$$\eta_{TH} = a_0 - a_1 \times \left(\frac{T_{F,MEAN} - T_A}{G} \right) \quad (eq. 5)$$

Relations between the 1D-model and the linear formula

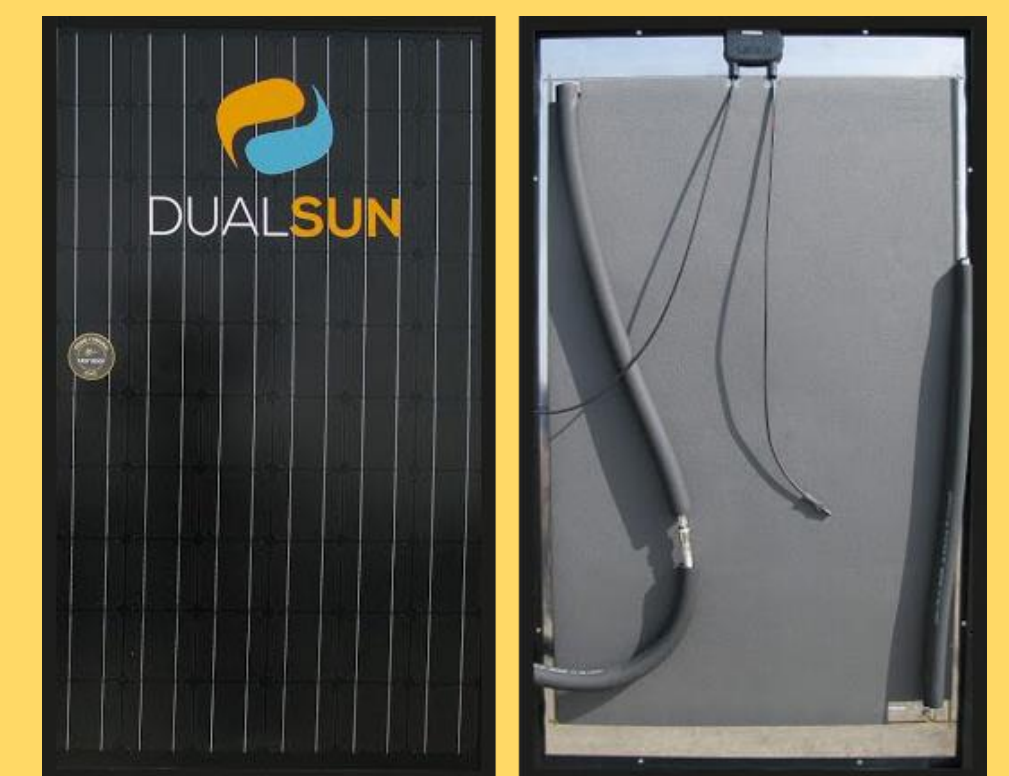
$$a_0 = \frac{\dot{m} \cdot Cp \cdot D \cdot Width \cdot (C - T_A)}{G \cdot Area} \quad (eq. 6)$$

$$a_1 = \frac{\dot{m} \cdot Cp \cdot D \cdot Width}{Area} \quad (eq. 7)$$

Prototypes and testing

Description of the constitutive layers for the 9 prototypes tested

	Glass	EVA	Cells	EVA	BS	EVA	Stainless Steel Heat exchanger / PV surface	Insulation (equivalent thickness given for k=0.033W/(m.K))
	mm	mm	-	mm	mm	mm	-	mm_equiv
1	2	0.6	60 (MPPT)	1.2	0.4	1.2	74%	NO
2	2	0.6	60 (OC)	1.2	0.4	1.2	74%	NO
3	2	0.6	60 (MPPT)	1.2	0.4	1.2	74%	39.6mm
4	2	0.6	60 (MPPT)	1.2	0.4	1.2	74%	24.8mm
5	2	0.6	60 (MPPT)	0.6	0.4	0.6	74%	NO
6	4 & Low E	0.6	60 (MPPT)	1.2	0.4	1.2	74%	NO
7	2	-	-	0.6	0.4	0.6	74%	NO
8	-	-	-	-	-	-	exch only	NO
9	2	0.6	40 (OC)	1.2	0.4	1.2	100%	NO



Ex of prototype (1669*982mm²)

Pictures of the artificial sunlight test bench (1000W/m², wind speed 1.5m/s, T_{F,in}=20..70°C)



Photovoltaic and thermal results for the 9 prototypes

	a0 (%)	a1 (W/K/m ²)	Wp *	β _{WP} (%/°C)	a0 (%)	a1 (W/K/m ²)	Wp *	β _{WP} (%/°C)	
1	50.2%	12.8	238	-0.048	6	49.8%	13.0	225	-0.050
2	59.9%	13.1	-	-	7	66.1%	13.3	-	-
3	49.6%	10.6	238	-0.050	8	39.8%	11.3	-	-
4	49.8%	11.4	238	-0.050	9	75.7%	17.9	-	-
5	52.8%	13.1	245	-0.055					

*limiting cell equivalent power at 1000W/m² and 25°C

Model validation

Introduction of two new factors in the model

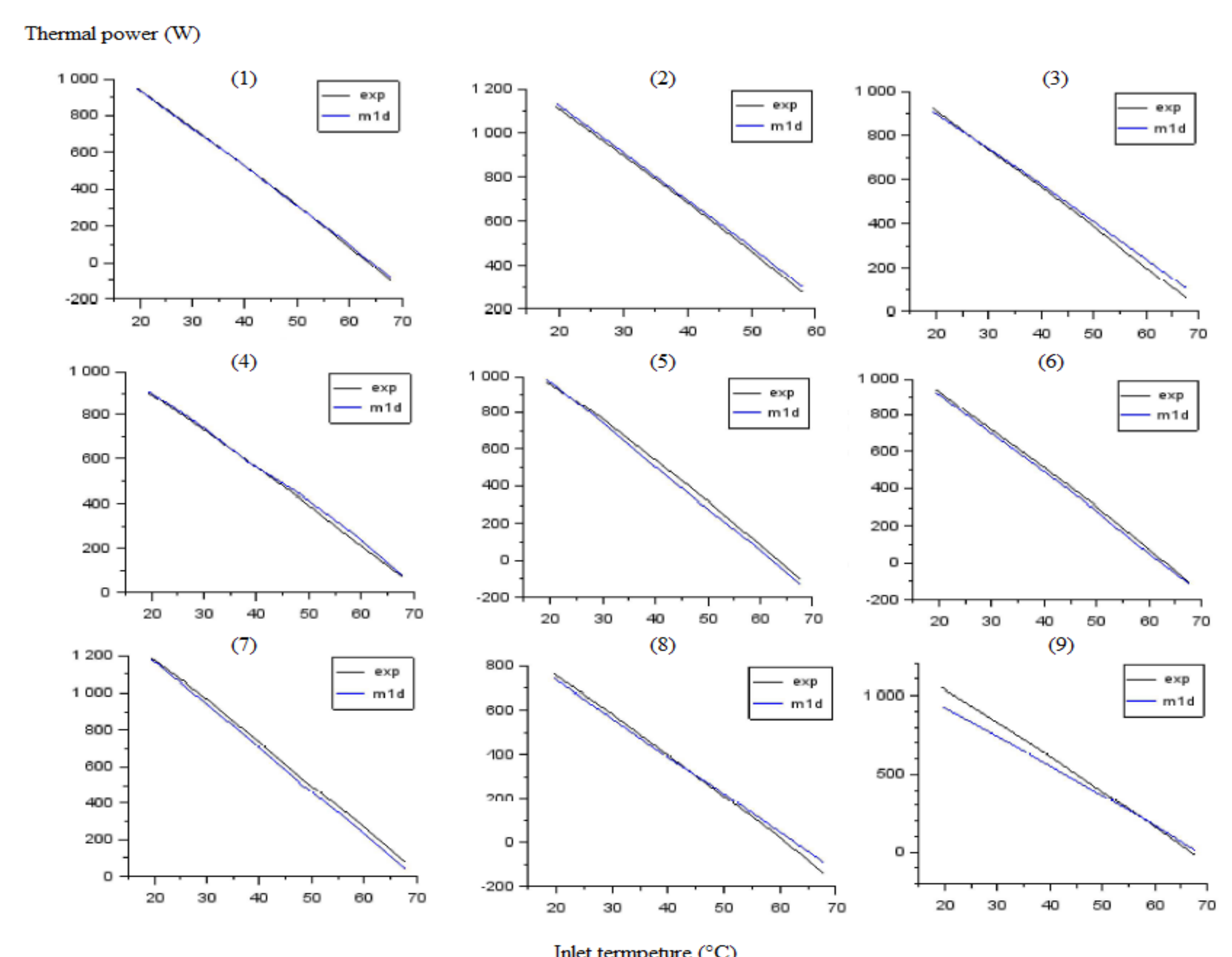
Two parameters were introduced to take better into account for the specific behavior of the Dualsun stainless steel heat exchanger :

- Effect of the fin
⇒ Correction of the ratio Stainless Steel Heat exchanger / PV surface 82% instead of 74%
- Unknown heat exchange between the fluid and the stainless steel (which was supposed fixed at 800 W/(m².K))
⇒ Correction of the length of exchange 770mm instead of 856mm

Root-mean-square error for each model/ test fitting with the corrected model

Test	1	2	3	4	5	6	7	8	9
RMSE	8.74	17.14	26.39	15.09	29.98	20.33	28.35	25.42	66.98

Visualization of model and experimental results



The simplified model (1D) gives a good fit with the 9 first prototypes performance results. These encouraging results must be confirmed with further tests with a polymeric heat exchanger.